

Calculations:

The cantilever system can be modeled as a beam of midline length L , width $W(x)$, and thickness $T(x)$. It is assumed to have uniform density p and Young's Modulus E . The function $y(x,t)$ represents the position of the cantilever midline along the y -axis, and the cantilever is fixed so that $y(0,t)=0$ and $y'(0,t)=0$. The system can be analyzed by considering the forces on any arbitrarily small width-wise section of length dx , and thickness du . The forces in question are tension and shear, $F(x)$ and $F(y)$ respectively. F_x arises from the bending of the material and its bulk elasticity. F_y arises from the fact that the plank must remain a single, continuous piece. Over the bent section indicated by dx ,

$$\Delta x = \frac{R+u}{R} dx - dx = \frac{U}{R} dy$$

Where R is given by the second derivative for $y(x)$.

$$y - y_0 = \frac{1}{2} y'' dx^2$$

$$R^2 = dx^2 + (y_0 + \frac{1}{2} y'' dx^2)^2$$

Because $R = y_0$,

$$0 = dx^2 + Ry'' dx^2 + \theta(dx^2)^2$$

$$y'' = -\frac{1}{R}$$

$$R = -\frac{1}{y''}$$

$$\Delta x = -uy'' dx$$

For the plank to remain continuous, there must be present both shear ($S(x)$) and torque. These can be represented as the derivatives in respect to time of each other and $y(x)$.

$$S(x - dx) = S(x) + \frac{d^2 y}{dx^2} dm$$

$$\Gamma(x - dx) = \Gamma(x) + S(x) dx$$

This indicates that $S' = -pWT \frac{d^2 y}{dx^2}$, $\Gamma' = -S$ and $\Gamma'' = pWT \frac{d^2 y}{dx^2}$. By balancing these equations for force we can define an equation from which we can derive a solution.

$$E \frac{d^2}{dx^2} (WT^3 \frac{d^2 y}{dx^2}) = -pWT \frac{d^2 y}{dx^2}$$

This fourth-order differential equation shows similarities to general wave equations, and because of this can support wave-like solutions. A system of conditions is required to solve for a particular solution in all cases; These can be found from the system boundary conditions.

The first scenario assumes the simplest possibility: that the plank width W and thickness T are constant. Simplifying the general equation under these conditions gives

$$\frac{d^4 y}{dx^4} = -\left(\frac{p}{ET^2}\right) \frac{d^2 y}{dt^2}$$

Because of the oscillatory properties of the plank's vibration, it is given that

$$y = y_0 e^{i(kx - \theta t)}$$

As part of the definition of the eigenmode, $y(x,t)$ can be further partitioned into the product of two separate one-variable equations.

$$y(x,t) = y_a(x) e^{i\theta t}$$

This allows y to be defined as an eigenfunction in the following equation

$$\frac{d^4 y_a}{dx^4} = \left(\frac{p}{ET^2}\right) \theta^2 y_a$$

Where the fourth derivative is a linear Hermitian operator which returns the function multiplied by a scalar, equivalent to the the constant term. Because it is Hermitian, it is possible to build a general solution for this equation using a linear combination of terms which satisfy certain conditions.

$$y_a = a_1 e^{ikx} + a_2 e^{-ikx} + a_3 e^{kx} + a_4 e^{-kx}$$

$$k = \left(\frac{p\theta^2}{ET^2}\right)^{\frac{1}{4}}$$

Using the four known boundary conditions, a system of equations can be developed to solve for the constant coefficients. The boundary conditions are:

$$y_a(0) = y'_a(0) = 0$$

$$y''_a(L) = y'''_a(L) = 0$$

These make the following system of equations.

$$a_1 + a_2 + a_3 + a_4 = 0$$

$$i(a_1 - a_2) + (a_3 - a_4) = 0$$

$$-a_1 e^{ikL} - a_2 e^{-ikL} + a_3 e^{kL} + a_4 e^{-kL} = 0$$

$$-ia_1 e^{ikL} + ia_2 e^{-ikL} + a_3 e^{kL} - a_4 e^{-kL} = 0$$

Because this is a homogenous system of equations, there exist solution sets only for specific values of k . Each set represents a different eigenmode in the plank's vibration. It is possible to solve for k by considering the matrix system created by these four equations.

$$\begin{bmatrix} a_1 & a_2 & a_3 & a_4 \\ ia_1 & -ia_2 & a_3 & -a_4 \\ -e^{ikL} & -e^{-ikL} & e^{kL} & e^{-kL} \\ -ie^{ikL} & ie^{-ikL} & e^{kL} & -e^{-kL} \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

The determinant of the augmented matrix must be zero, because it is singular. If we let $a = e^{ikL}$ and $b = e^{kL}$, then the determinant is:

$$\begin{aligned} 8i + \frac{2i}{ab} + \frac{2ib}{a} + \frac{21a}{b} + 2iab &= 0 \\ 4ab + 1 + b^2 + a^2 + a^2b^2 &= 0 \\ (a + b)^2 + (ab + 1)^2 &= 0 \end{aligned}$$

There are no possible real solutions for (a, b) ; a must be complex. If $a = e^{i\omega}$, then:

$$\begin{aligned} a_r + b &= \pm a_i b \\ a_r b + 1 &= \mp a_i \\ a_r &= \frac{-2b}{b^2 + 1} \\ a_i &= \pm \frac{1 - b^2}{1 + b^2} \end{aligned}$$

Leading to the following identity, which allows a series of k values to be solved for, each of which corresponds to a different eigenmode.

$$\omega = \arctan \frac{b^2 - 1}{2b} = \pm \ln b$$

$$k = 1.8751, 4.6941, 7.8532, 10.9955, 14.1372, 17.2788, 20.4204, 23.5619, \dots$$

Note: Omega here does not mean frequency, as it does elsewhere.

It is now possible to solve for the constants in the solutions to the differential equation by substituting each k value into the homogenous matrix of boundary conditions above and determining the values of a_1, a_2, a_3 and a_4 .

For the case of non-uniform width, the values of the constants in the solutions can be found from the original equation. For example, for a diamond shaped cantilever with length equal to its width:

$$\begin{aligned} \frac{dW}{dx} &= \begin{cases} 2 & 0 \leq x \leq \frac{L}{2} \\ -2 & \frac{L}{2} \leq x \leq L \end{cases} \\ (2x) \frac{d^4 y}{dx^4} + (4) \frac{d^3 y}{dx^3} - \Omega(2x)y &= 0 \end{aligned}$$

$$\frac{d^4 y}{dx^4} + \frac{2}{x} \frac{d^3 y}{dx^3} - \Omega y = 0$$

This equation can be symbolized using the following operators:

$$H = H_0 + H'$$

And can be solved for the necessary constants using the following steps.

$$y_i^{(4)} = \Omega \omega^2 y_i$$

$$H_0 y_i = e_i y_i$$

$$H = H_0 + H'$$

$$Hy(x) = H \sum_i c_i y_i(x) = \epsilon y(x)$$

$$\sum_i c_i (Hy_i)$$

$$\sum_i c_i (H_0 y_i + H' y_i)$$

$$\sum_i c_i \epsilon y_i = \sum_i c_i e_i y_i + \sum_i c_i H' y_i$$

$$(y_j, y_i) = \delta_{ij}$$

$$(y_j, H' y_i) = H'_{ij}$$

$$c_j \epsilon = c_j e_j + \sum_i c_i H'_{ij}$$

$$H'_{ij} c_i = c_j (\epsilon - e_j)$$

$$(H'_{ij} + e_j \delta_{ij}) c_i = \epsilon c_j$$

$$(H'_{ji} + e_i \delta_{ji}) c_j = \epsilon c_i$$