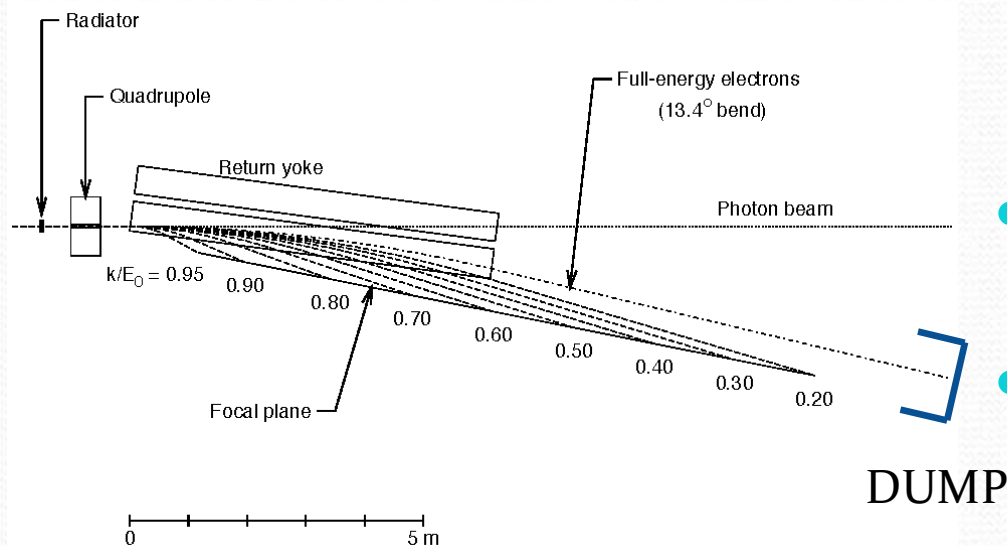


# Tagger Magnet Requirements

Jim Stewart (JLAB)  
Internal Magnet Review  
May 2009

# Magnet Requirements:

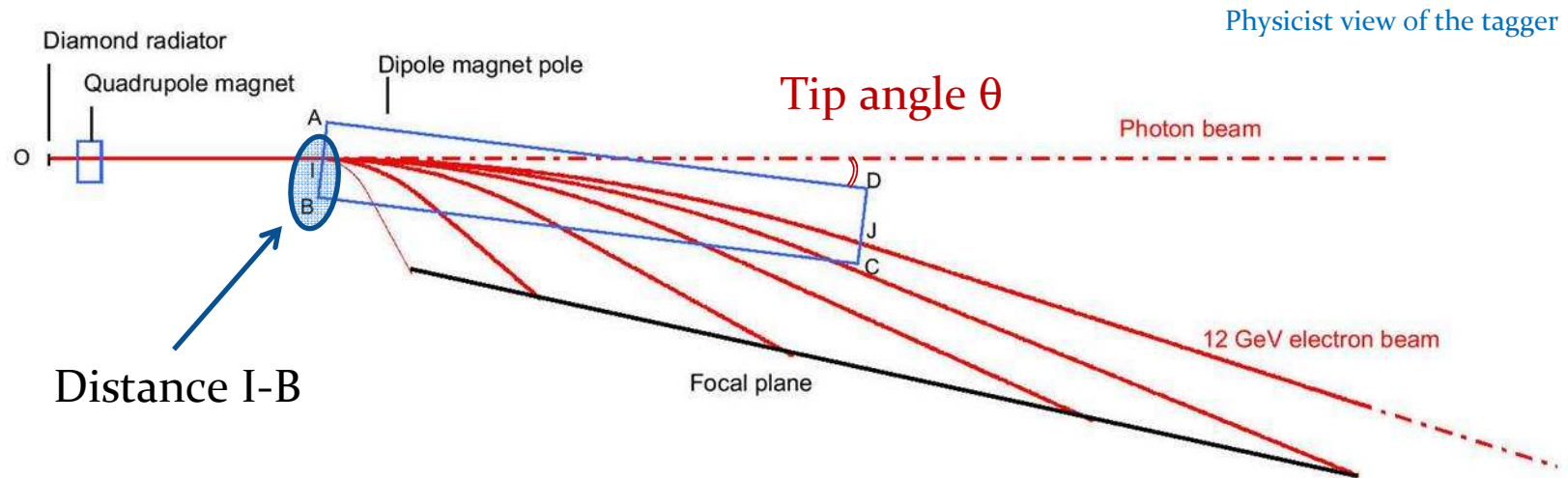


- The magnet must bend the electron beam  $13.4^\circ$  to the dump
  - Given 1.5 T then  $L_{\text{eff}} = 6.3\text{m}$
- The photon beam must pass through undisturbed
- The shape of the field must allow accurate measurement of the electron energy along the focal plane.

# Spectrometer Specification

- Photon energy detection from 70 to 75% of  $E_0$  with a resolution of 0.5%.
  - For a 12 GeV beam this implies the photon energy range 8.4 to 9 GeV.
  - Resolution set by physics and the GlueX momentum resolution.
- Detector capable of  $5 \times 10^6$  electrons/s per 0.1% of the above photon range.
- Additional capability to detect photons in the range 25 to 97% of  $E_0$  (3 to 11.7 GeV for  $E_0=12$  GeV)

# Uniform field optimization



- Optimize distance I-B and magnet tip angle  $\theta$  using transport (Glasgow).
- Best Results
  - I-B = 210 mm and  $\theta = 6.5^\circ$

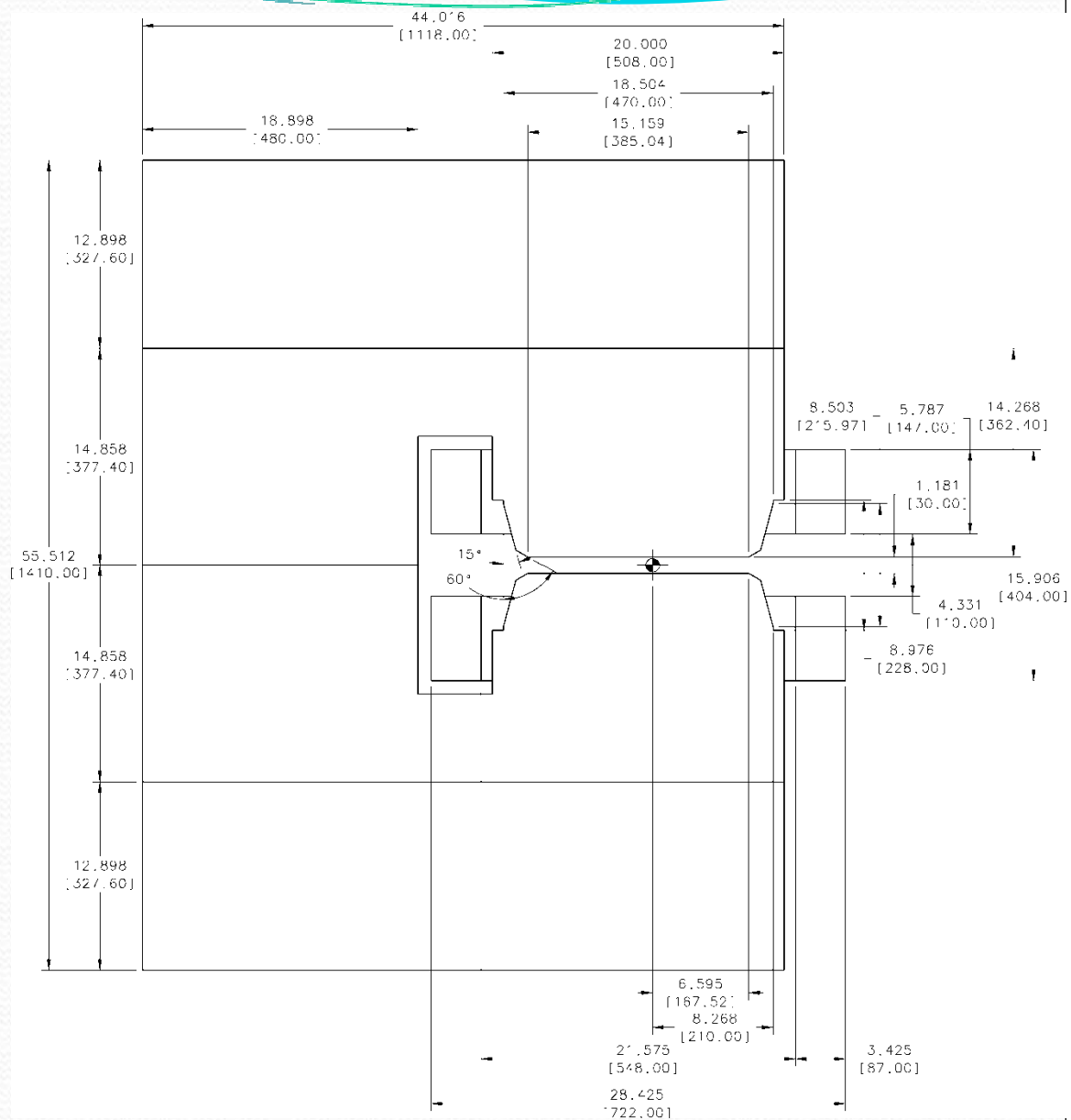
# More Detailed Simulations

Magnet with the geometry shown on the right was modeled in Tosca and ANSYS.

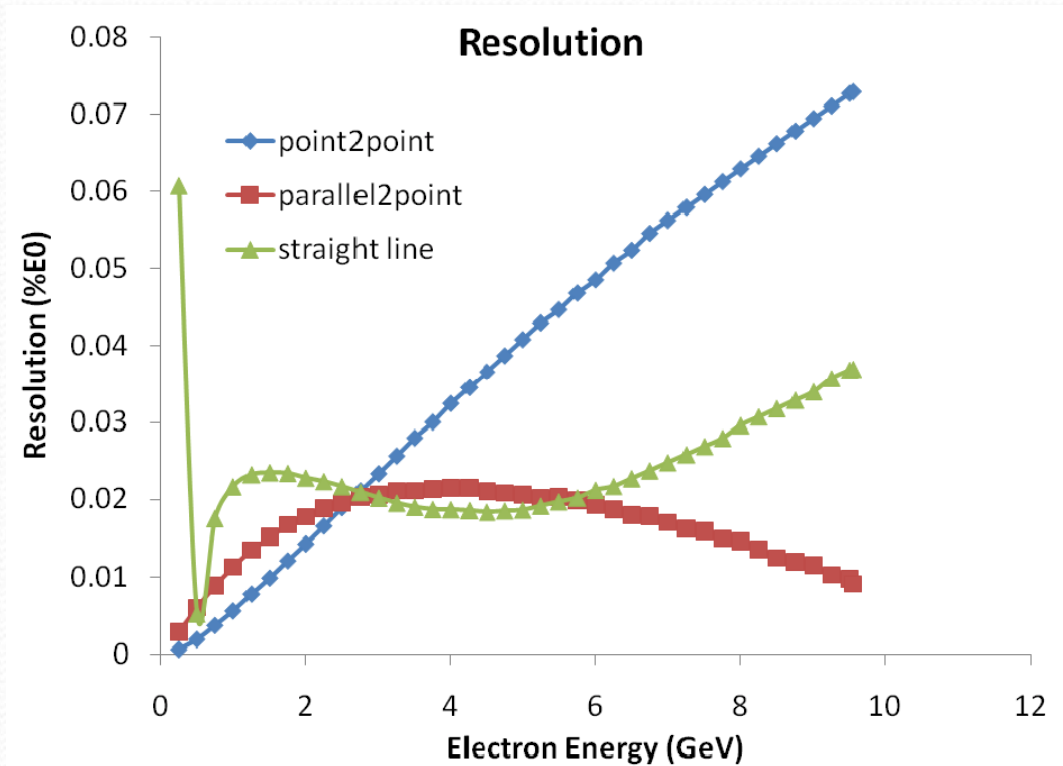
The computed fields agreed well with each other.

In TOSCA particles were tracked through the magnet and the image on the detector plane was determined.

The TOSCA field was inserted into GEANT and the tracking results were cross checked.



# Excellent Intrinsic Resolution Achievable



TOSCA  
RESULTS

Intrinsic resolution much better than 0.5% requirement from GlueX  
Do not want to exclude future high precision experiments!

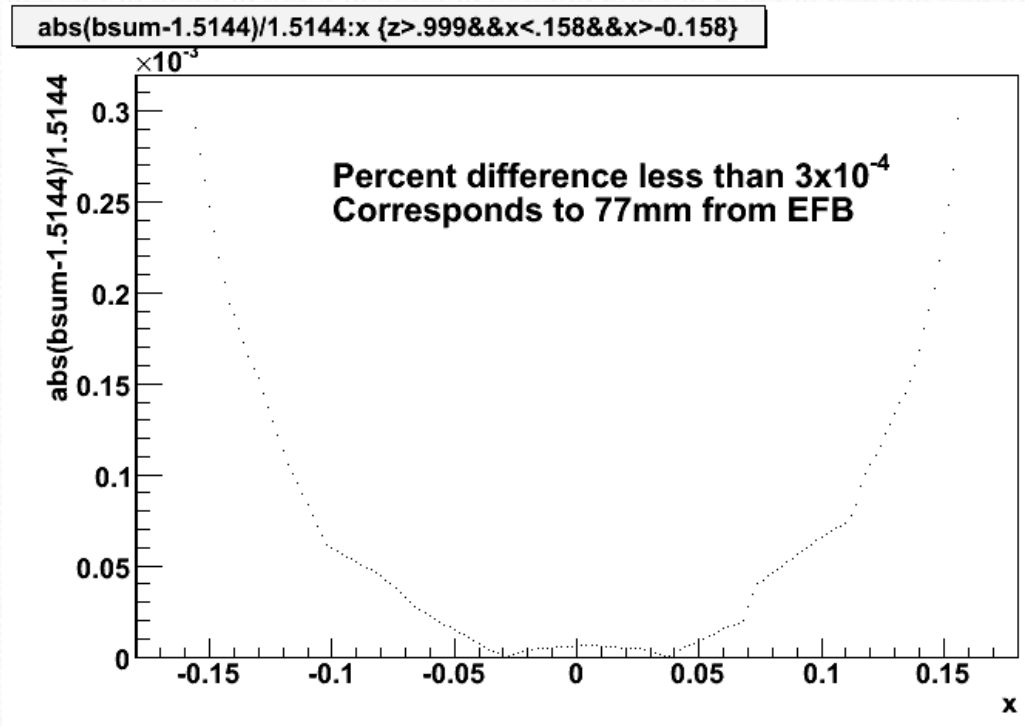
# Use this to set a uniformity Spec!

Zoom in on central field region.

Plot the fractional change in the field relative to the central field.

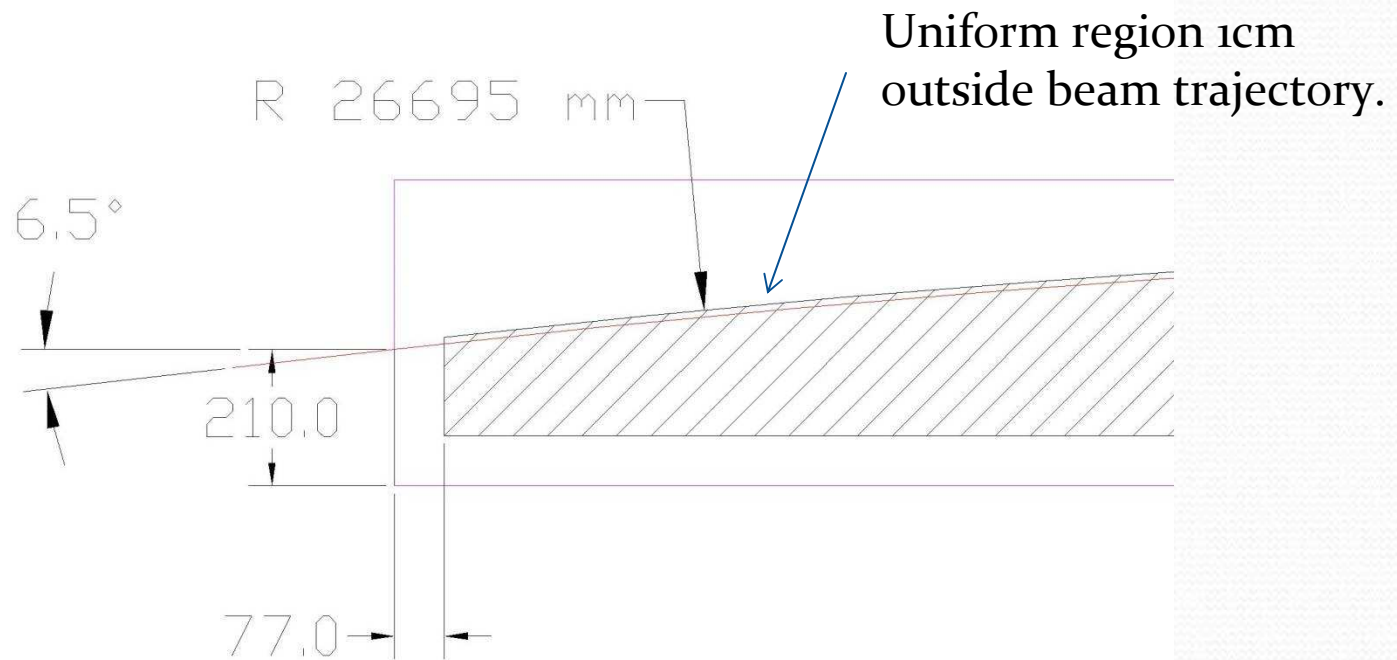
Determine that 77 mm in from the Effective Field Boundary (EFB) the uniformity has reached the level of  $3 \times 10^{-4}$ .

This resulted in the following uniformity SPEC.



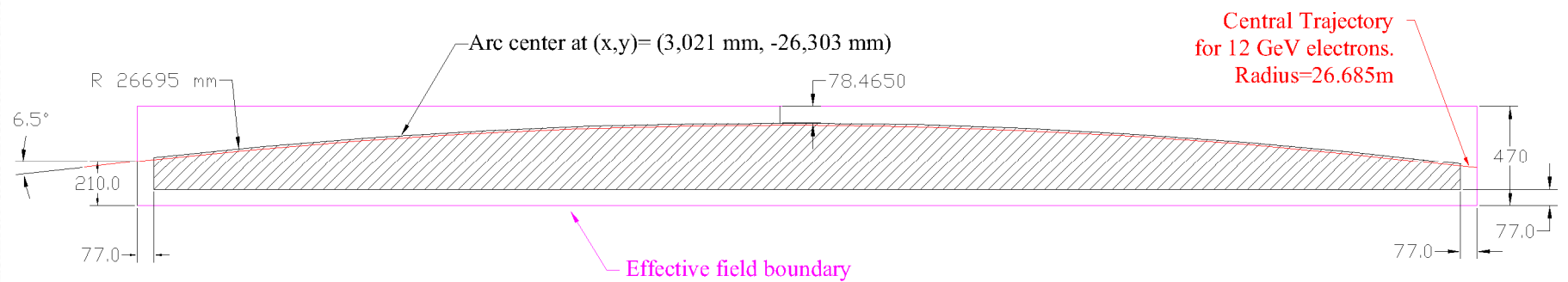
Field Profile from ANSYS

# Uniform field region





# Uniform Field region

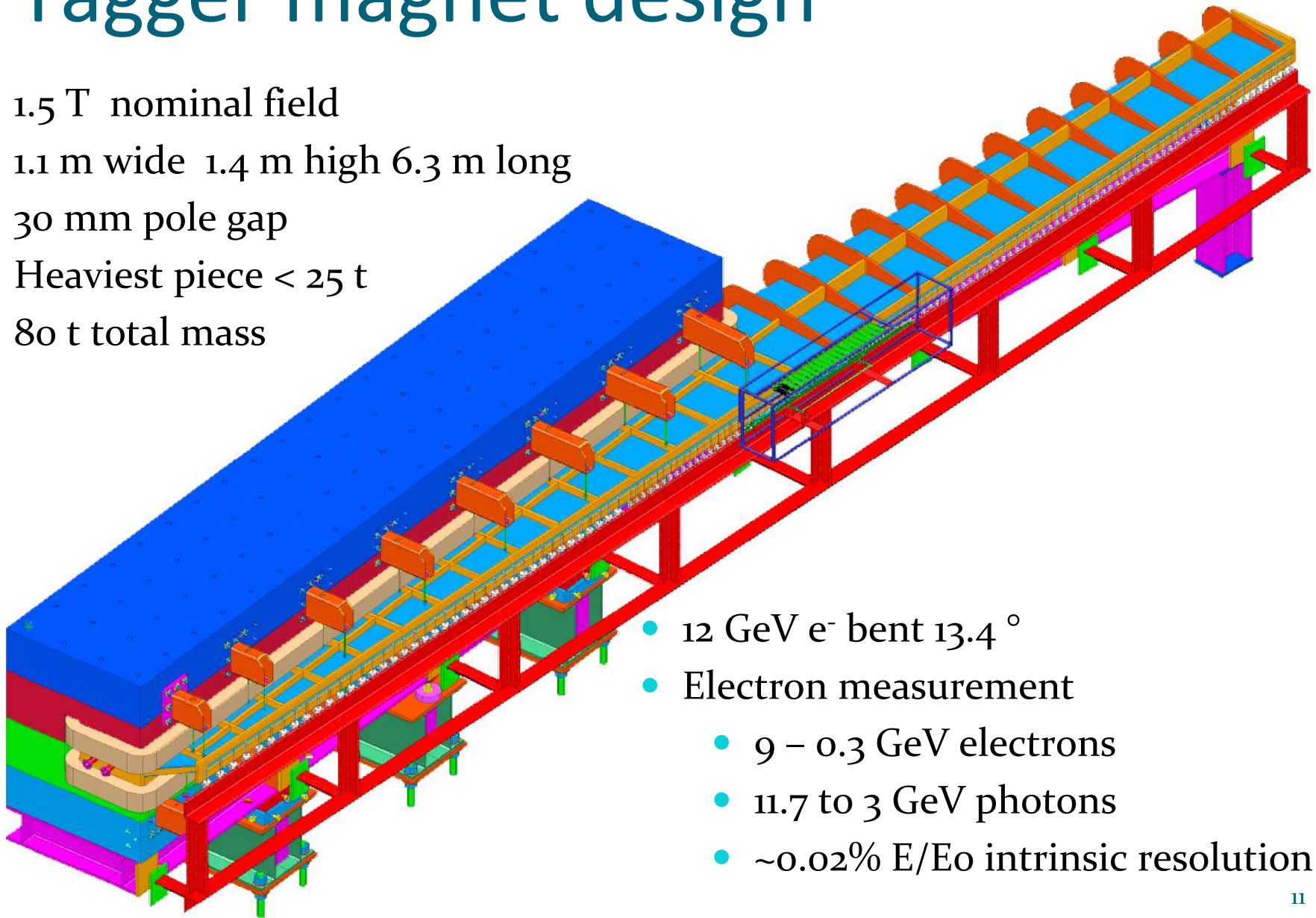


# Magnetic Technical Requirements

Requirement	Units	Value
Magnet Type		Normal conducting C-Magnet
Nominal magnetic field	T	1.500
Maximum magnetic field	T	1.80 (needed for hysteresis suppression)
Magnet Gap	mm	30
Effective Length @1.5T	mm	6,300 ± 2
Distance to -x effective field boundary @1.5T	mm	235± 2 Defined in drawing D00000-19-00-3002
Local uniformity volume		Defined in drawing D00000-19-00-3002 $3 \times 10^{-4}$ over 100 mm length in uniform region within +/- 2mm of horiz. plane
Global uniformity volume		Defined in drawing D00000-19-00-3002 Better than 1% in full uniform region

# Tagger magnet design

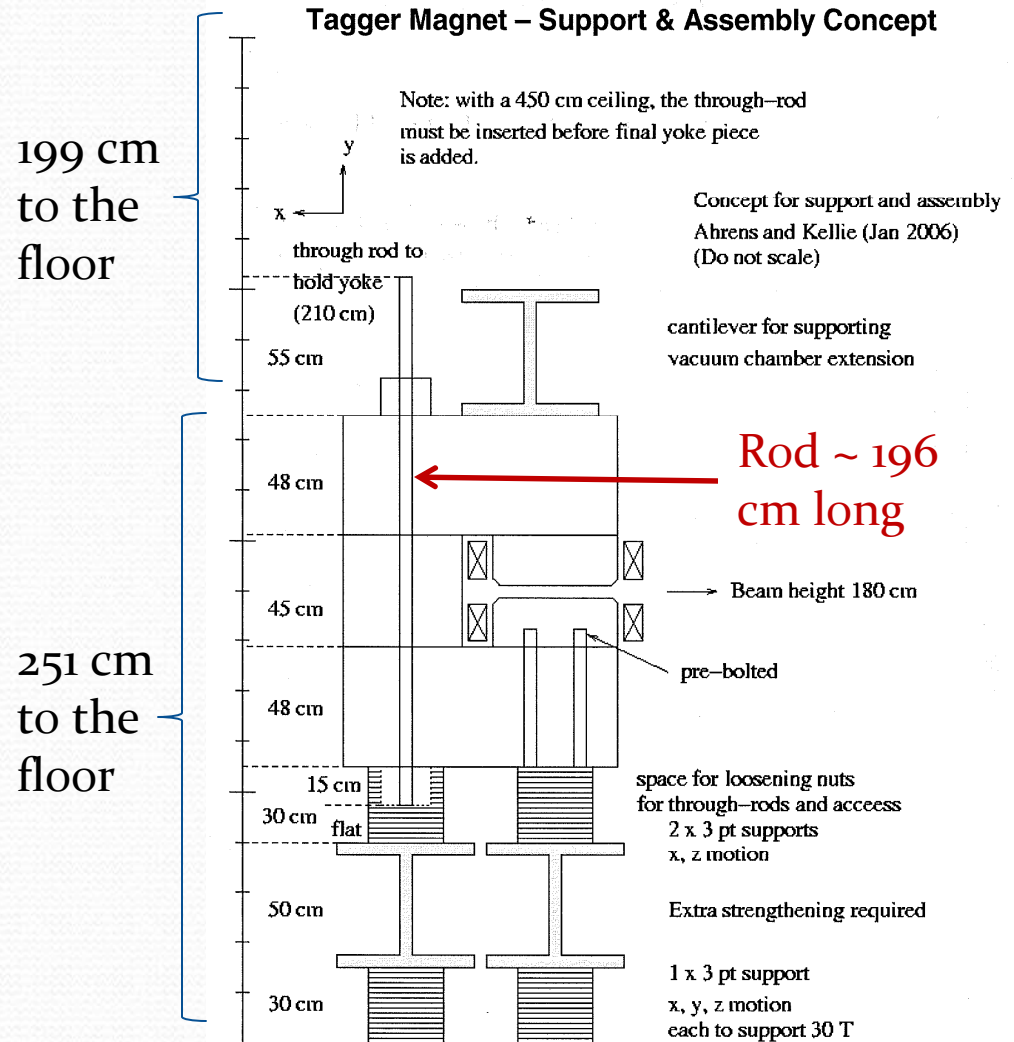
- 1.5 T nominal field
- 1.1 m wide 1.4 m high 6.3 m long
- 30 mm pole gap
- Heaviest piece < 25 t
- 80 t total mass



- 12 GeV  $e^-$  bent  $13.4^\circ$
- Electron measurement
  - 9 – 0.3 GeV electrons
  - 11.7 to 3 GeV photons
  - $\sim 0.02\%$   $E/E_0$  intrinsic resolution!

# Mechanical Requirements

- The magnet must fit in the hall.
  - Requires a space requirements drawing.
- It must be possible to assemble it.
  - Plan to have a 25 t gantry crane over the magnet.
  - Heaviest assembly must be under 25 t.
- Must fit in the hall.
  - Checked largest truck can back to the hall doors.



From Space Requirements document

# Magnet Mechanical Requirements

- Pole surface must be planar and parallel to  $\pm 0.1$  mm.
- The sealing surfaces to the vacuum chamber must be planar and parallel to  $\pm 0.2$  mm.
- No voids larger than 0.3" within 0.9" of the pole surface.
- Material, Heat treatment, and handling must be described at the time of the proposal.
- Vacuum wetted surfaces must be Ni plated.
- Fiducial features must be mounted as specified.
- Materials must be documented and the pieces marked.

# Mechanical requirements - Stands

- Must have correct height.
- Adjustment capability  $\pm 10$  mm hor.  $\pm 9$  mm vert.
- Minimum factor of 3 safety
- Documentation detailing safety analysis
- Welding in accordance with AWS D1.1
- Features to mount the detector package must be provided above the alignment cartridges
  - Needs described on an interface drawing.

# Coil Requirements

Requirements	Units	Value
Coil Mechanical Requirements		Drawings D00000-19-00-2010 and D00000-19-00-2010  winding scheme, fittings, brazing, material. Flags, fittings and klixon should be on drawing.
Maximum Design Temperature	°C	95
Maximum operating temperature	°C	80
Maximum water pressure	PSI	120
Maximum water supply pressure drop	PSI	100
Maximum flow rate	GPM	20
Maximum water flow velocity	ft/sec	8
Maximum voltage drop across all coils connected in series for 1.8 T	V	170 ?? 220V
Maximum Current	A	400

# Material specifications

I copied the specifications from Robin Wines' specification #MAG0000000S0045 for the XP Dipole Magnet Coils.

The materials and quality control items were very well specified and I saw no reason why we should change this.

This means that only the dimensions of the copper, the array size, and the details of the terminations are left to the manufacturer. We need to specify the fittings and flag dimensions.



# Vacuum Chamber Requirements

- No material in the path of electrons in the energy range 9 – 0.3 GeV electrons
- 11.1 m window with no bracing which crosses the horizontal plane.
- Must fit together and seal against the pole. Vacuum tight to  $10^{-11}$  mbar l/s.
- Safety according to ASME B&PV code section II.
- Vacuum pumping ports according to ASME B&PV code section VIII or FEA calculation.
- Material DIN 1.4429 (SAE 316LN)

# Vacuum Cham. Requirements cont.

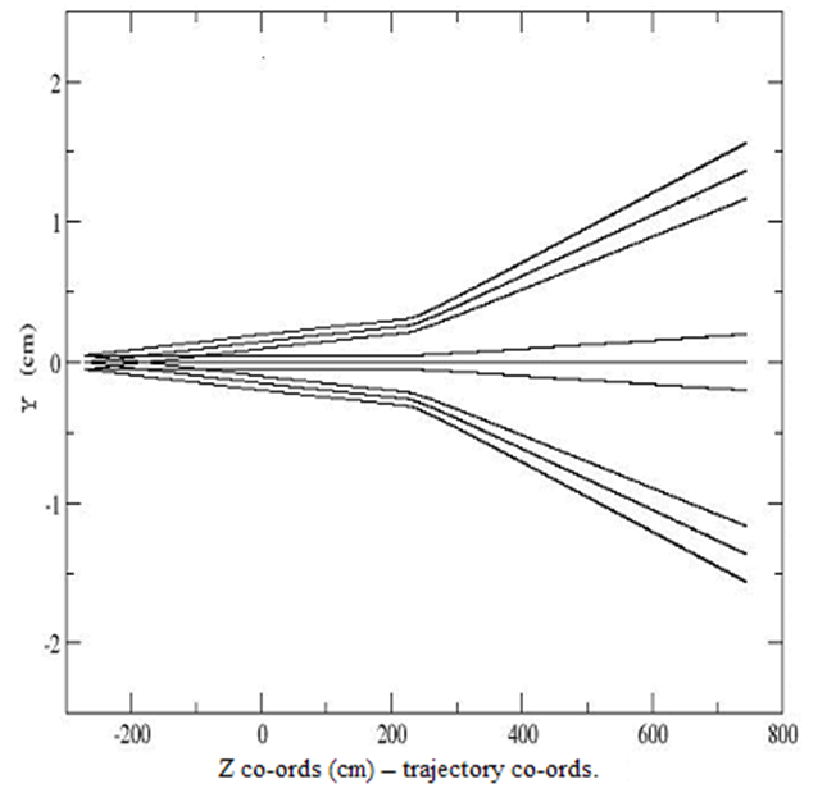
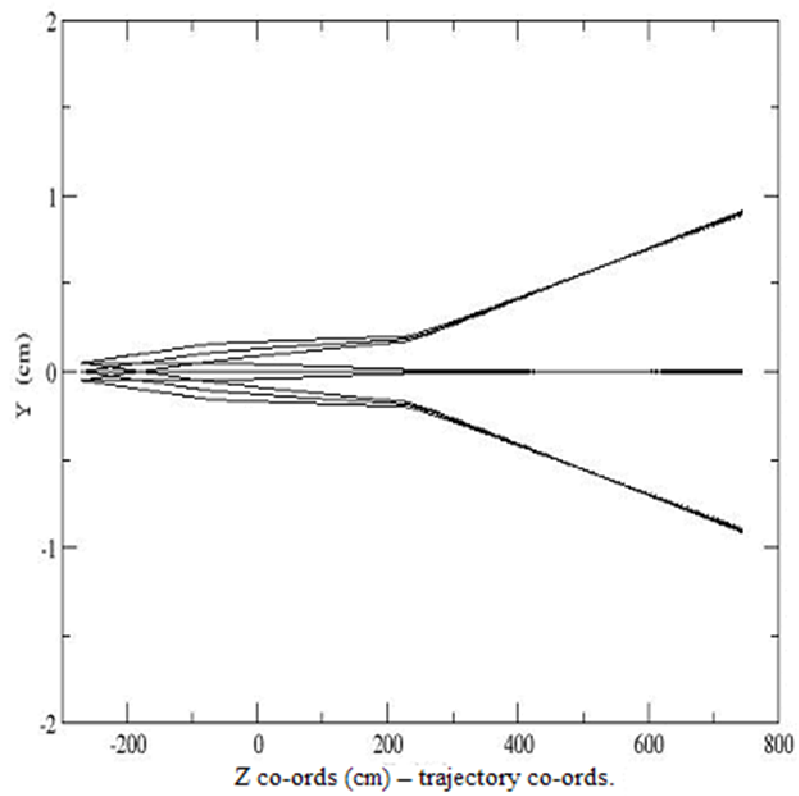
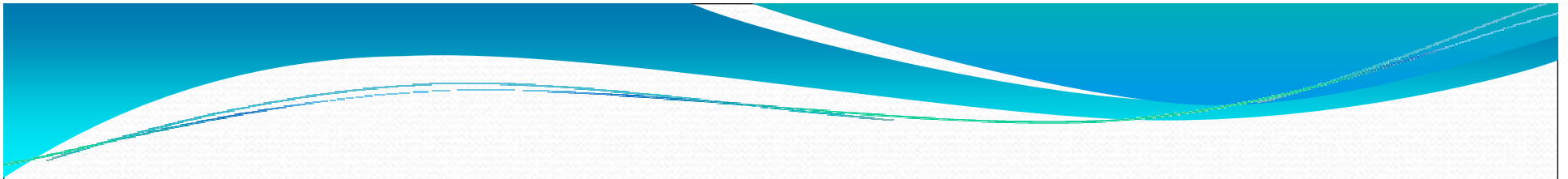
- Welding and inspection Specified in SOW
- Cleaning specified in SOW
- Require mechanical testing prior to assembly in the magnet.
- Lifting plan required for the chamber. Any tooling becomes property of JLAB.



Backup

# Manpower cost

- Mech Eng \$63.81 per hr
  - $63.81 * 40 * (52/44) = \$3.0 \text{ k per mw}$ 
    - Fully burdened non-escalated effort
- Mech Designer \$43.84 per hour
  - $\$43.84 * 40 * (52/44) = \$2.1 \text{ k per mw}$ 
    - Fully burdened non-escalated effort



## 2. The effects of the magnetic properties of stainless steel on the tagger performance.

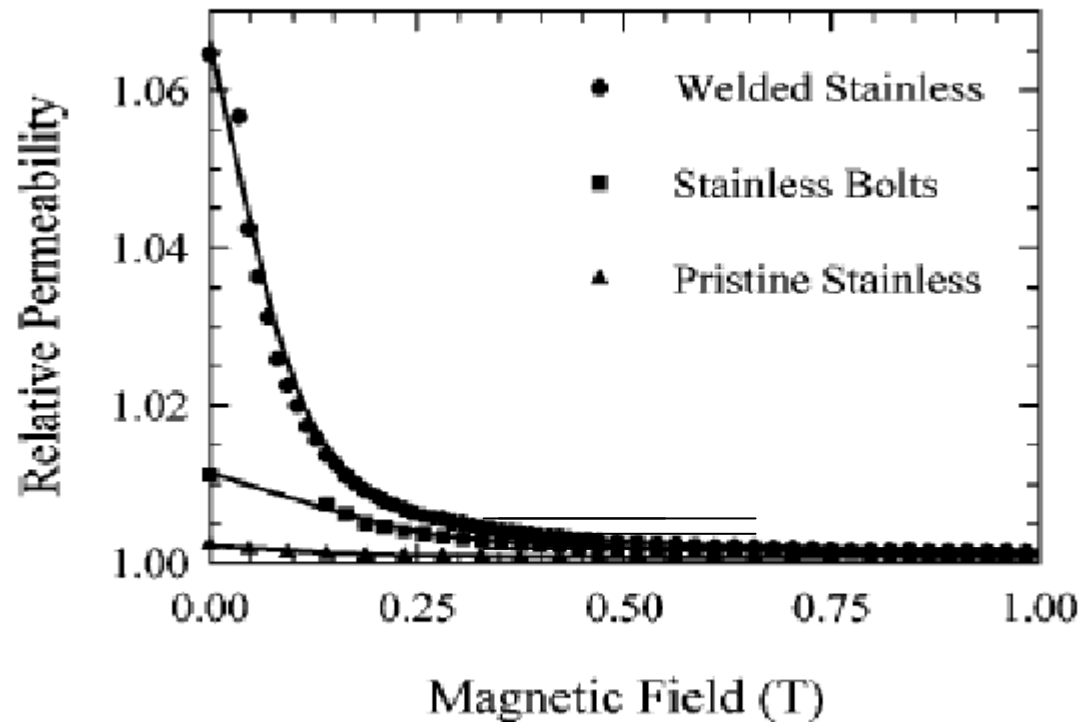


FIG. 3. Relative permeabilities as a function of applied magnetic field for welded, machined (bolts), and unwelded (pristine) 304 stainless steel.

(C. Weber and J. Fajans, Rev. Sci. Instrum., Vol. 69, No. 10, (1998) 3696)

The stainless steel used for the tagger vacuum chamber wall should be non magnetic stainless steel.

Type 304 and type 316 stainless steel are the most common materials used in accelerators.

Machining and welding can alter the properties of these steels.

Care must be taken to avoid undesirable effects on the vacuum chamber and the magnetic field distribution.