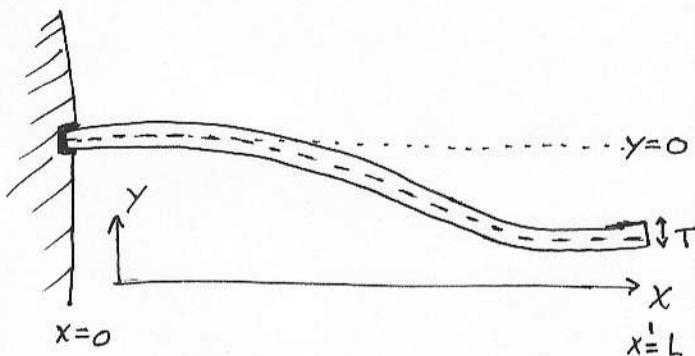


Q. What is the shape and frequency of  
a stiff sheet undergoing small-amplitude oscillations  
about a flat equilibrium geometry? Ignore gravity.

R. Jones

- \* Assumptions: the sheet is held fixed, with fixed slope, at one end, taken to be the left end. The right end is free, as shown below.

- \* Coordinate system:  $x, y$  axes, with origin, shown in the figure to the right.



- \* Dimensions: the plank is of length  $L$ , thickness  $T$ , width  $W$ , where  $T$  and  $W$  functions of  $x$  and not necessarily constants.

The plank is made of a uniform material of density  $\rho$  and bulk modulus  $E$ .

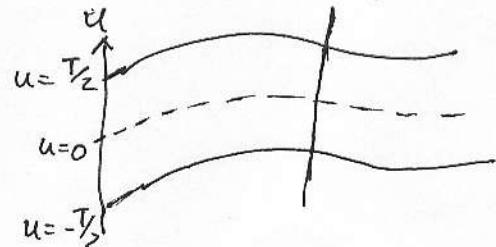
- \* Analysis of static forces at fixed displacement

Make an imaginary cut through the plank at  $x$  and ask what forces the part at the left places on that to the right

Let  $u$  measure depth inside the plank relative to the central layer.

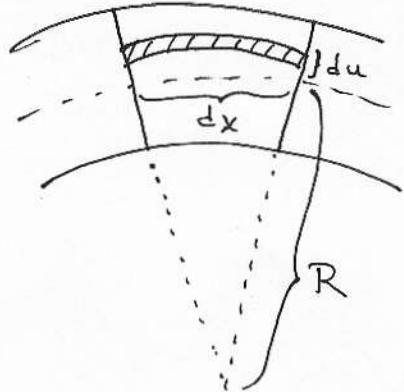
Forces are tension ( $F_x$ ) and shear

( $F_y$ ).  $F_x$  arises from bending of the material and its bulk elasticity.  $F_y$  arises from the fact that the plank remains a single continuous piece - it is a constraint in the problem.



To get  $F_x$ , consider a bent shape as shown to the right. The layer indicated by  $du$  is stretched from its equilibrium length  $dx$  by a distance

$$\Delta x = \left(\frac{R+u}{R}\right)dx - dx = \frac{u}{R}dx$$



What is  $R$ ? It is given by the second derivative for  $y(x)$

$$\text{Let } y - y_0 = \frac{1}{2}y''dx^2, \text{ then } R^2 = dx^2 + (y_0 + \frac{1}{2}y''dx^2)^2$$

$$\text{But } y_0 = R, \text{ so } R^2 = dx^2 + R^2 + Ry''dx^2 + O(dx^2)^2$$

$$\therefore y'' = -\frac{1}{R}, R = -\frac{1}{y''}$$

So  $\Delta x = -uy''dx$ . What is the force element from  $du$ ?

$$dF_x = E \frac{\Delta x}{dx} du = -WEuy''du$$

$$F_x = \int_{-T/2}^{T/2} \frac{dF_x}{du} du = -WEy'' \left( \frac{u^2}{2} \right) \Big|_{-T/2}^{T/2} = -\frac{1}{8}WEy''(T^2 - T^2) = 0$$

Forces cancel, but torques do not. Tension forces make torque

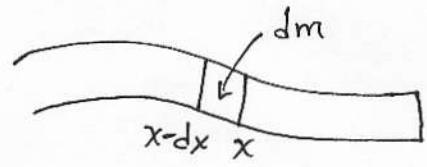
$$\Gamma = \int_{-T/2}^{T/2} \frac{dF_x}{du} u du = -WEy'' \left( \frac{u^3}{3} \right) \Big|_{-T/2}^{T/2} = -\frac{1}{12}WEy''T^3$$

To propagate this force along the plank, subject to the constraint that the plank remains intact, we need to keep track of both the shear  $S(x)$  and torque  $\Gamma(x)$  as we move along.

$$S(x - dx) = S(x) + \ddot{y}(x) dm$$

$$\Gamma(x - dx) = \Gamma(x) + S(x)dx$$

$$\begin{aligned} S' &= -\rho WT \ddot{y} \\ \Gamma' &= -S \end{aligned} \quad \left. \begin{aligned} \Gamma'' &= \rho WT \ddot{y} \end{aligned} \right\}$$



$$dm = \rho WT dx$$

assume "thin plank"  
 $L \gg T$

(3)

$$E \frac{d^2}{dx^2} \left( W T^3 \frac{dy}{dx^2} \right) = -\rho W T \frac{d^2 y}{dt^2}$$

This is not a wave equation because it is fourth order in  $x$ , but it can support wave-like solutions under certain conditions.

Case a) Let  $W, T$  be constants, then  $W$  drops out!

$$\frac{d^4 y}{dx^4} = -\left(\frac{\rho}{ET^2}\right) \frac{d^2 y}{dt^2}$$

$$\text{Let } y = y_0 e^{i(kx - \omega t)}, \quad k^4 y_0 = \frac{\rho \omega^2}{ET^2} y_0$$

Boundary conditions are  $y = y' = 0 @ x=0$   
 $y'' = y''' = 0 @ x=L$

Normal mode condition:  $y(x,t) = y(x) e^{i\omega t}$

$$\frac{d^4 y}{dx^4} = +\left(\frac{\rho}{ET^2}\right) \omega^2 y$$

$$y = y_1 e^{ikx} + y_2 e^{-ikx} + y_3 e^{kx} + y_4 e^{-kx}, \quad k = \left(\frac{\rho \omega^2}{ET^2}\right)^{1/4}$$

$$\textcircled{1} \quad y_1 + y_2 + y_3 + y_4 = 0$$

$$\textcircled{2} \quad i(y_1 - y_2) + (y_3 - y_4) = 0$$

$$\textcircled{3} \quad -iy_1 e^{ikL} - y_2 e^{-ikL} + y_3 e^{kL} + y_4 e^{-kL} = 0$$

$$\textcircled{4} \quad -iy_1 e^{ikL} + iy_2 e^{-ikL} + y_3 e^{kL} - y_4 e^{-kL} = 0$$

These equations are homogeneous, so solutions only exist subject to certain constraints on  $k$  (or  $\omega$ ). This is what gives the eigenmode equation.

$$\begin{vmatrix} 1 & 1 & 1 & 1 \\ i & -i & 1 & -1 \\ -e^{ikL} & -e^{-ikL} & e^{kL} & e^{-kL} \\ -ie^{ikL} & ie^{-ikL} & e^{kL} & -e^{-kL} \end{vmatrix} = 0$$

Let  $a = e^{ikL}$ ,  $b = e^{kL}$

$$\begin{aligned}
 &= \left\{ -i [-1-1] - 1 \left[ \frac{1}{ab} - \frac{i}{ab} \right] - 1 \left[ -\frac{b}{a} - i \frac{b}{a} \right] \right\} \\
 &\quad - \left\{ i [-1-1] - 1 \left[ \frac{a}{b} + i \frac{a}{b} \right] - 1 [-ab + iab] \right\} \\
 &\quad + \left\{ i \left[ \frac{1}{ab} - \frac{i}{ab} \right] + i \left[ \frac{a}{b} + i \frac{a}{b} \right] - 1 [-i - i] \right\} \\
 &\quad - \left\{ i \left[ -\frac{b}{a} - i \frac{b}{a} \right] + i [-ab + iab] + 1 [-i - i] \right\} \\
 &= 8i + \frac{2i}{ab} + \frac{2ib}{a} + \frac{2ia}{b} + 2iab
 \end{aligned}$$

$$\therefore 4ab + 1 + b^2 + a^2 + a^2b^2 = 0$$

$$(a+b)^2 + (ab+1)^2 = 0$$

$\therefore a=1, b=-1$  or  $a=-1, b=1$ , neither one is possible!

or  $a$  is complex! in fact, it is a pure phase  $e^{i\phi_a}$

$(ab+1) = \pm i(a+b)$ ,  $b$  is pure real,  $b > 1$ .

$$\begin{cases} a_r + b = \pm a_i b \\ a_r b + 1 = \mp a_i \end{cases} \quad \frac{a_r}{b} + a_r b + 2 = 0 \Rightarrow a_r = -\frac{2b}{b^2+1}$$

$$\textcircled{*} \quad \phi_a = \tan^{-1}\left(\frac{a_i}{a_r}\right) = \boxed{\tan^{-1}\left(\frac{b^2-1}{2b}\right)} = \pm \ln b$$

$$a_i = \pm \frac{1-b^2}{1+b^2}$$